



Magnetically Levitated 6 DoF Controlled Sample Manipulator for Tomography

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Mocraf Workshop

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Partners in Mechatronic Innovation

R&D company, supporting innovation at our customers
with the focus on high-end mechatronic systems and products.

Founded in 2007

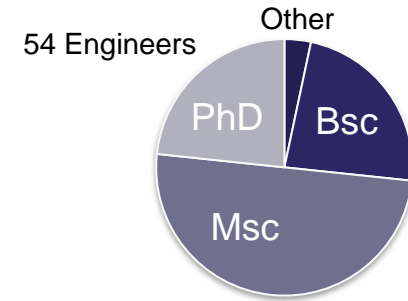
Located in the Eindhoven region, The Netherlands

- Cleanrooms, Temp controlled enclosures, low-nose floor, ...

Market segments, professional production equipment

- Semiconductor (Wafer scanners, die-bonders)
- Analytical and imaging (Electron microscopes)
-
- Scientific instrumentation (Synchrotron beamlines equipment)

Booth: C02

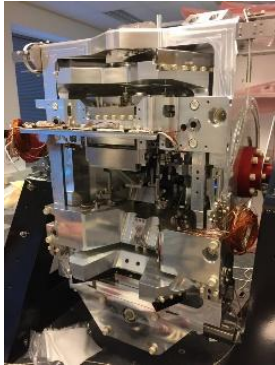


From quasi-static to high dynamic positioning

Trent in beamline equipment:

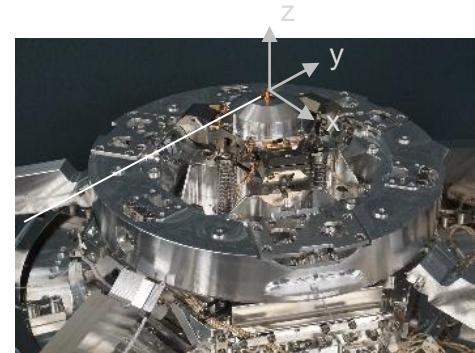
1. Higher accuracy: from sub-micron to nm
2. Faster: from quasi-static position to high dynamic scanning applications
3. Cleaner: not only UHV but also low-outgassing of C_xH_y to keep optics clean

High-dynamic DCM with nrad performance during fly scan (LNLS)



The High-Dynamic Double-Crystal Monochromator (Ph.D. Renan Geraldes, 2023)

Sample manipulator (x,y,z,Rz) with fast raster xz-scanning (LNLS)



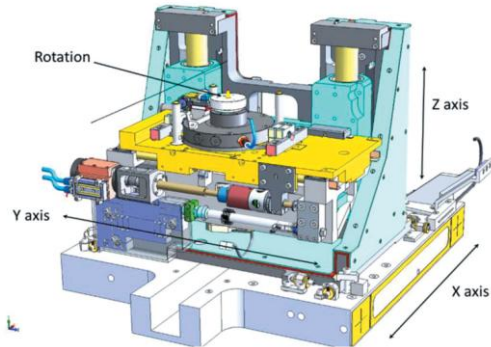
TUOBM02

Way of approach: Mechatronic system design

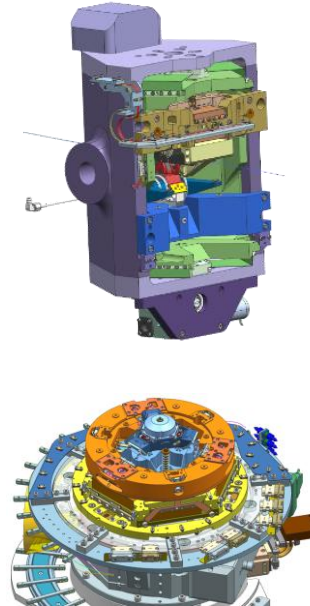
Stacking of multiple “standard 1DoF” motion stage $\xrightarrow{\text{Fast and nm}}$

Limitations:

- Limited stability and repeatability
- Lack of metrology, very indirect metrology loop with many uncontrolled DoF
- Limited dynamics performance
- Not UHV compatible, high CxHy outgassing



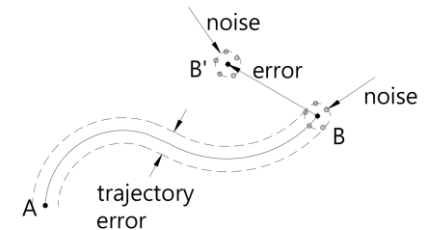
Source: Gema Martínez-Criado et al. J. Synchrotron Rad. (2016)



Dedicated (Mechatronic) system design

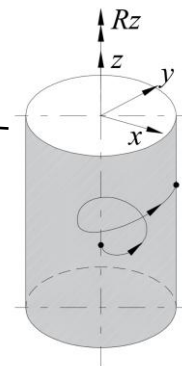
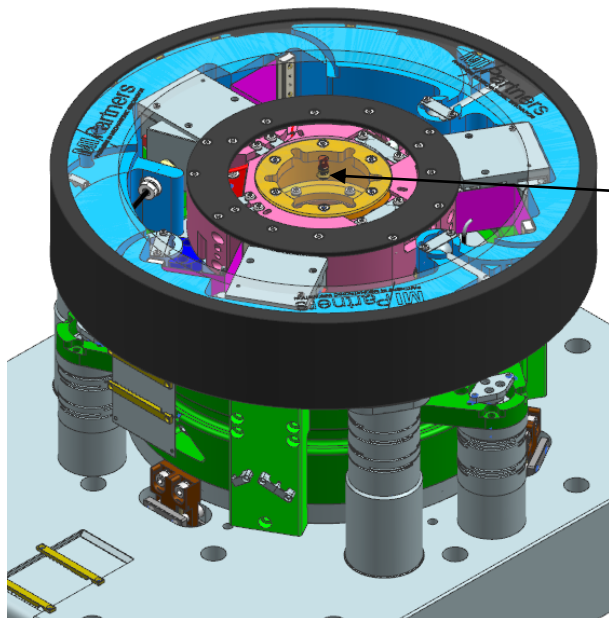
Benefit:

- Direct control and metrology of all essential DoF
→ high stability and repeatability
- Optimize design: stiff and low mass
→ High mechanical eigenfrequencies and servo band with high disturbance rejection and tracking performance
- Short/optimal metrology loop
→ high (thermal) stability
- UHV design, control of outgassing components, cleaning,
-



Magnetically Levitated 6 DOF Manipulator

Single step 6 DoF motion stage with precise 6 DoF metrology for e.g. tomography



Arbitrary scanning motions
simultaneously $[x, y, z, R_z]$:
(spiral, raster,)

Stokes:
 x, y, z : 3 mm
 R_z : continuously
 R_x, R_y : ≈ 0 (2 mrad)

Velocities:
 x, y, z : 50 mm/s (limited by metrology resolution)
 R_z : 5 Hz (depending on offset)

Accelerations:
 x, y, z : 2 m/s²

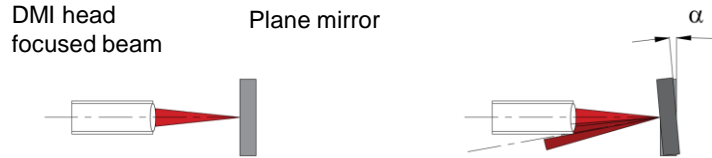
Metrology and motion performance:
 x, y, z : 5 nm (RMS)
 R_x, R_y : 20 nrad (RMS)
 R_z : 50 nrad (RMS)

- Position Metrology
- System Overview
- Actuator Design
- Control Architecture
- Positioning Performance

Metrology challenge

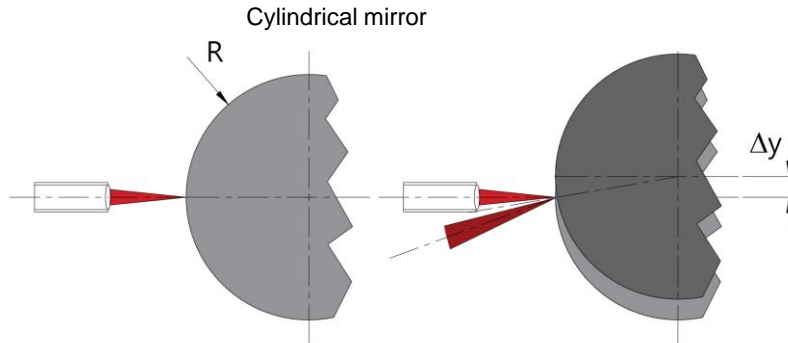
Position metrology in high-end stages typically by Distance Metrology Interferometer (DMI):

- High resolution/accuracy with long travel ranges
- Angular alignment limitations in “plane mirror” configuration



Angular range is very limited: typical $0.1 \dots 0.3^\circ$

Tomography manipulator continues Rz: rotation symmetric DMI target



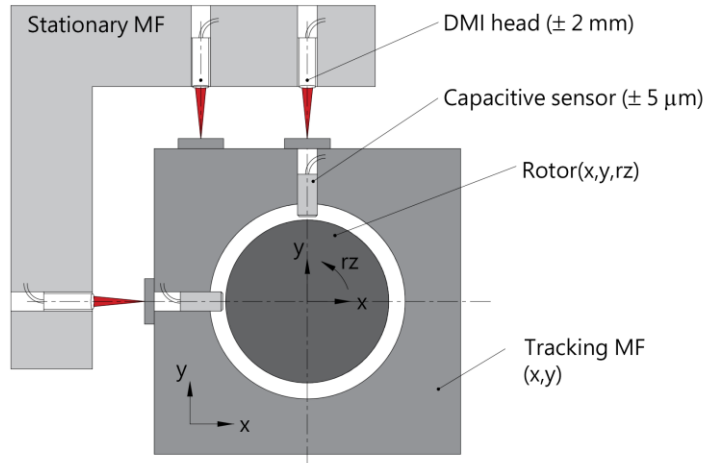
Offset of cylindrical mirror is very limited: $0.1 \dots 0.3 \text{ mm}$

$$\Delta y = R \tan(\alpha); R \approx 50 \text{ mm}$$

Metrology with Tracking Metrology Frame

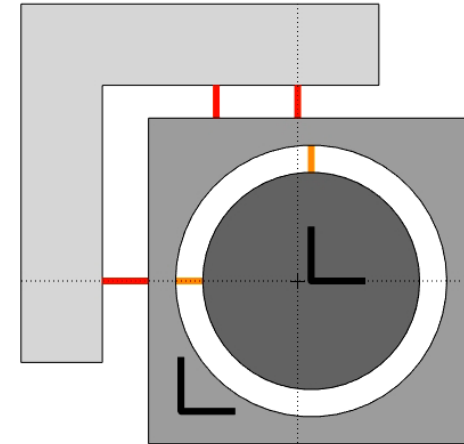
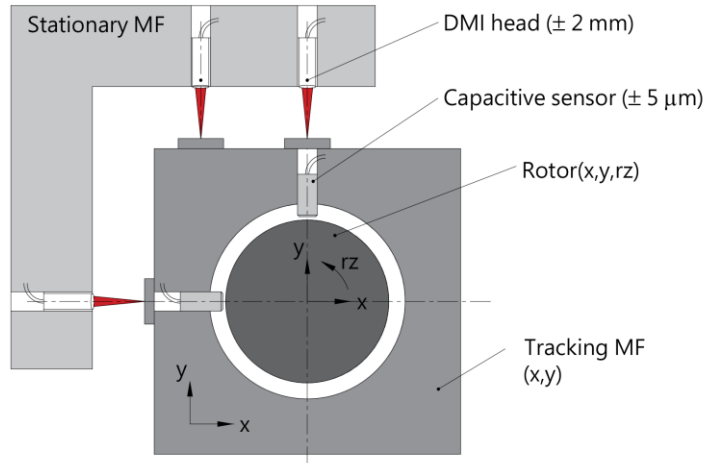
To allow large translations of the rotor: intermediate tracking metrology frame is used

1. Large motion between Stationary MF and Tracking MF measured by DMI (± 2 mm)
2. Small tracking error between Tracking MF and rotor ($\sim 5 \dots 10$ nm)

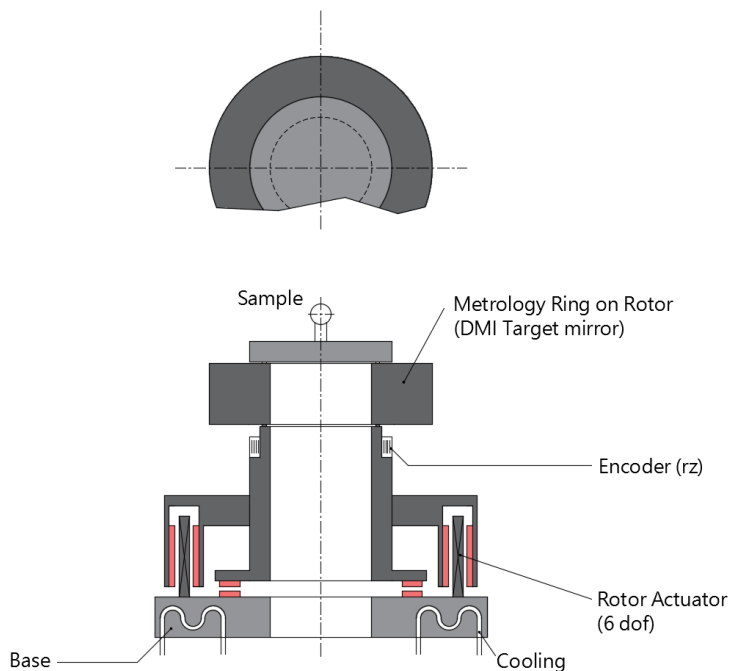


To allow large translations of the rotor: intermediate tracking metrology frame is used

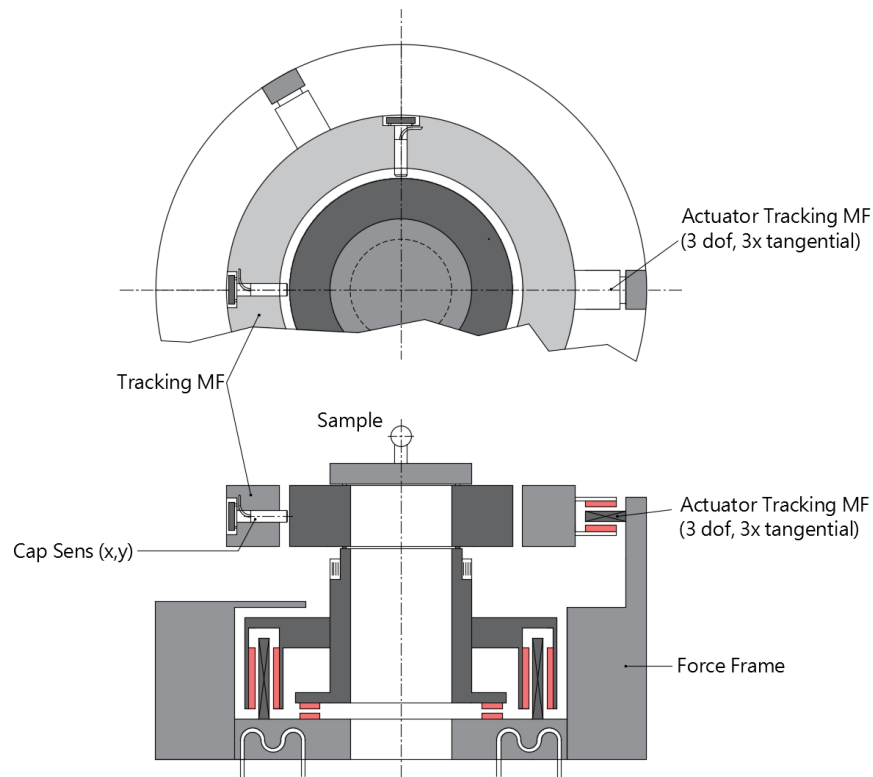
1. Large motion between Stationary MF and Tracking MF measured by DMI (± 2 mm)
2. Small tracking error between Tracking MF and rotor (± 1 μm)



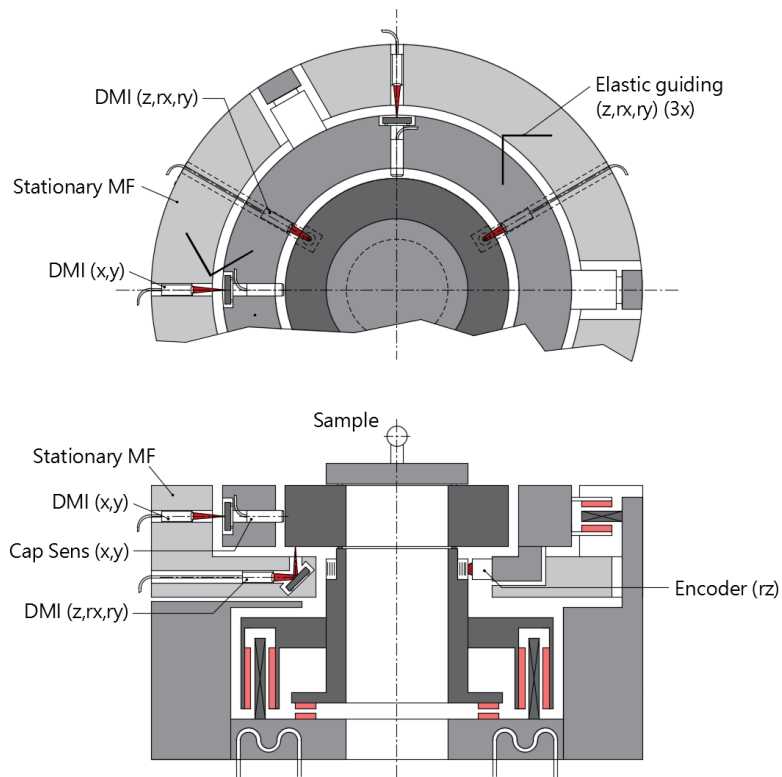
Actuation: Rotor with Actuator and Metrology Ring (DMI target)



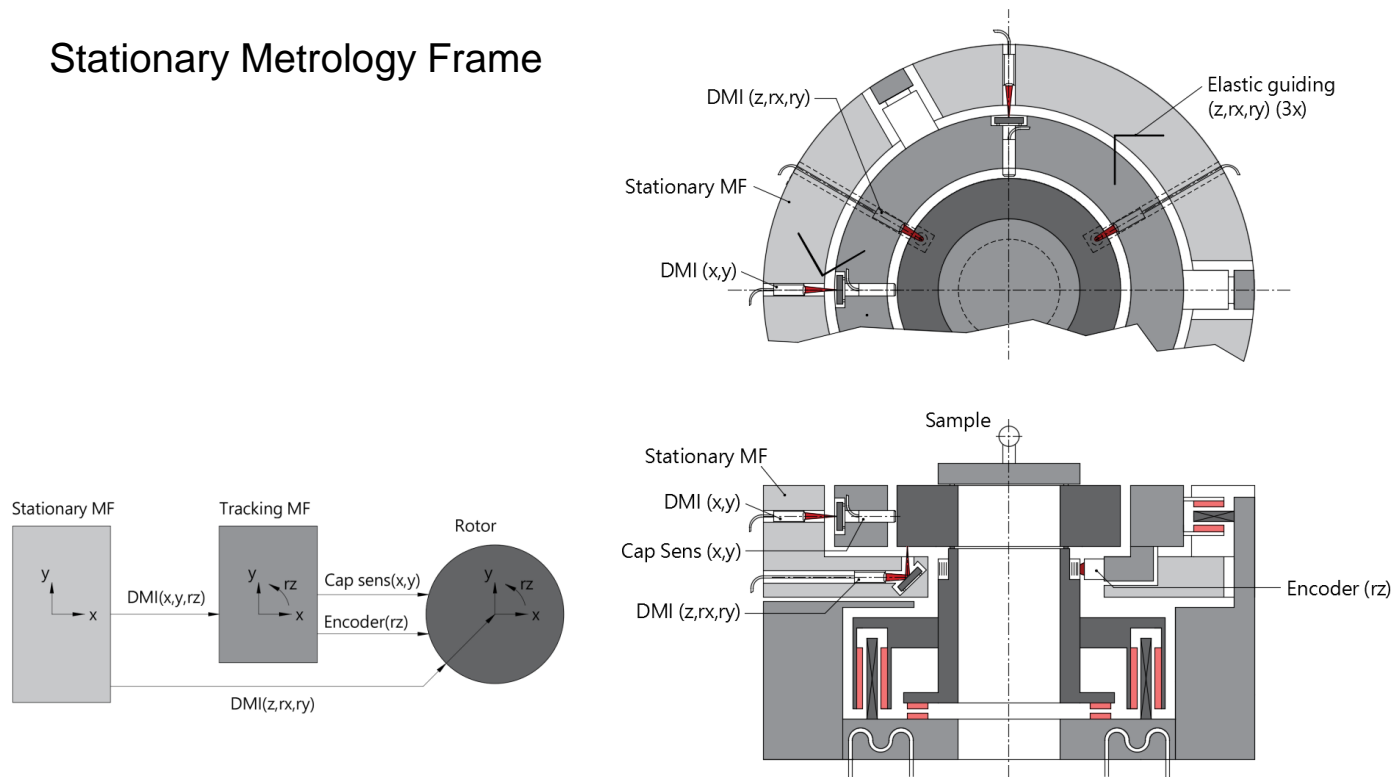
Tracking Metrology Frame



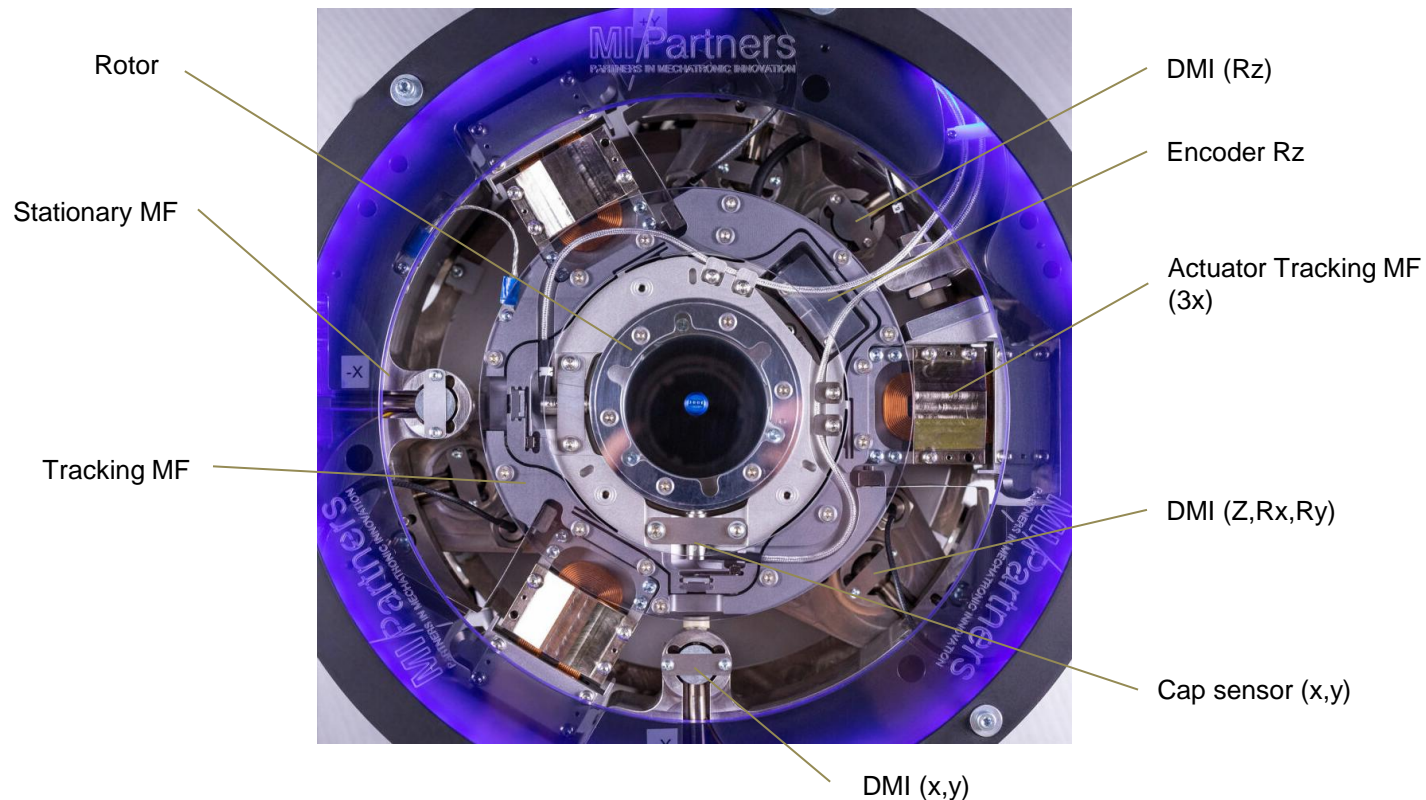
Stationary Metrology Frame



Stationary Metrology Frame

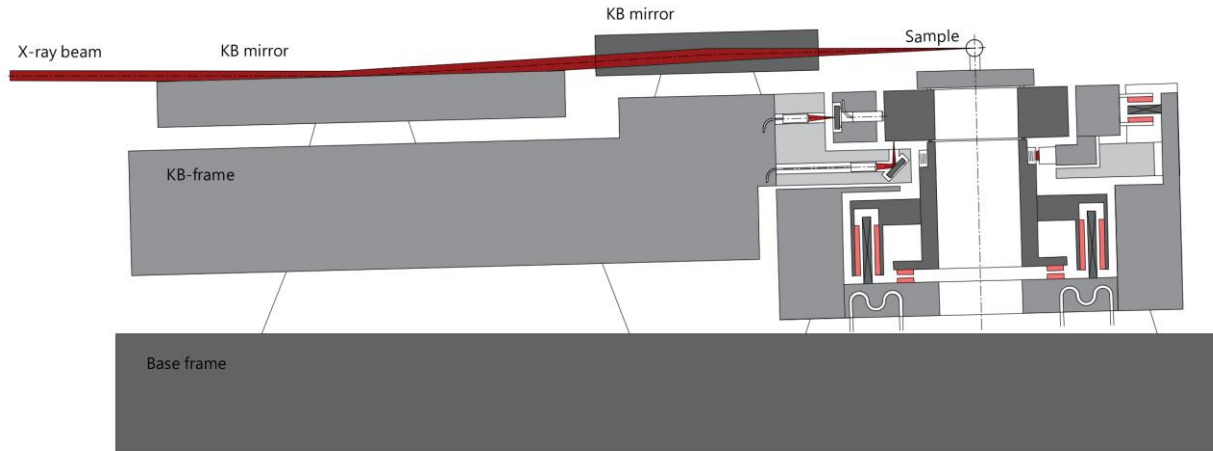


System Overview: Metrology

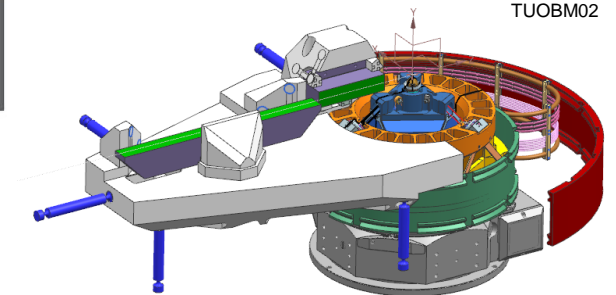


Metrology towards X-ray beam

Metrology frame integrated with dedicated KB frame: sample relative to X-ray beam

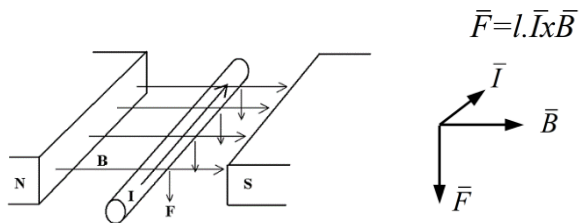


Example: Nanoprobe LNLS



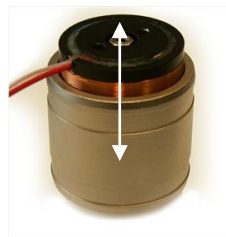
Actuation Principle: Lorentz forces

Lorentz force F

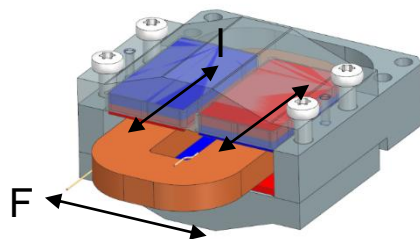
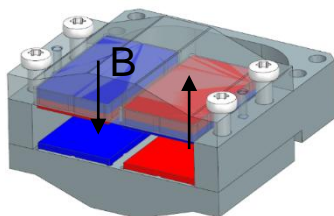


F

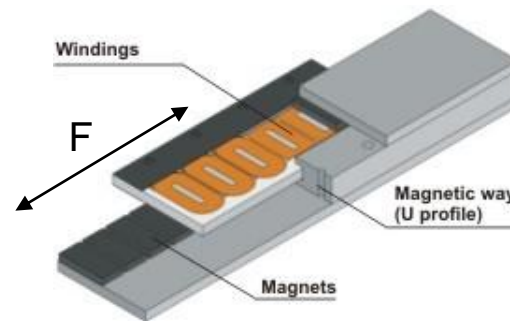
Voice coil actuator



1-phase actuator (small stroke)

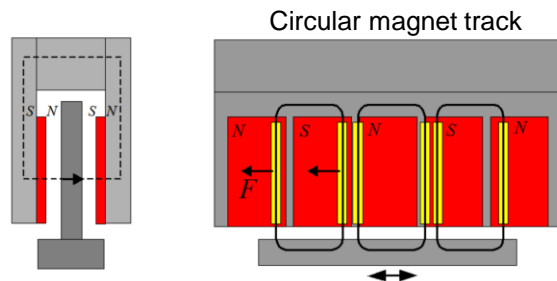


Iron-less linear actuator: 3-phase motor

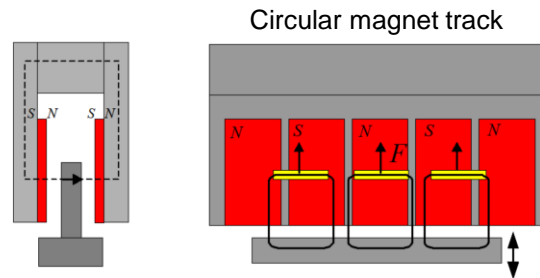


Actuation Principle: Tangential and axial force

Tangential force: 3-phase



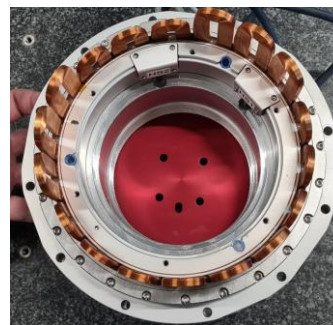
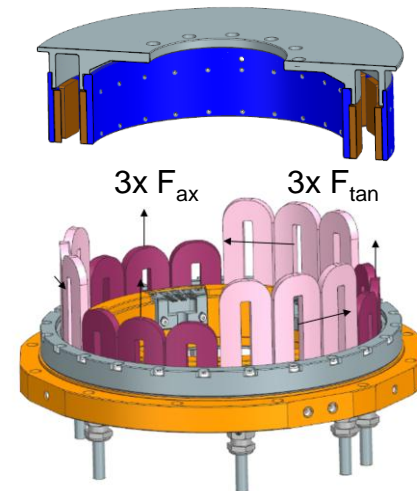
Axial force: 3-phase



Actuator assembly:

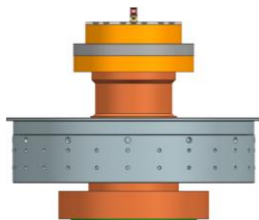
- 3x tangential force
- 3x axial force

Patent Pending

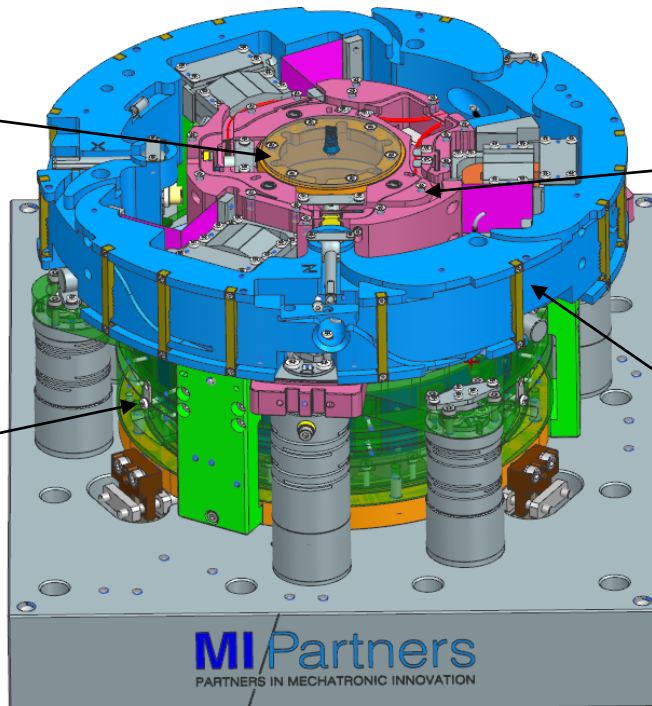
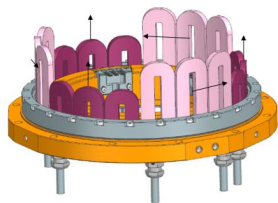


System Overview

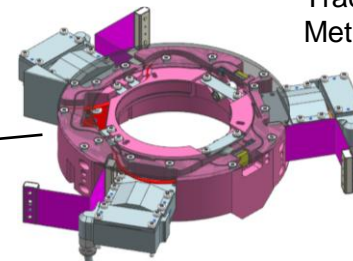
Rotor with metrology target
and actuator magnets



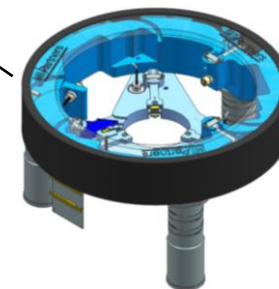
Actuator coils on force frame
active cooling (e.g. water)



Tracking
Metrology Frame



Stationary
Metrology Frame





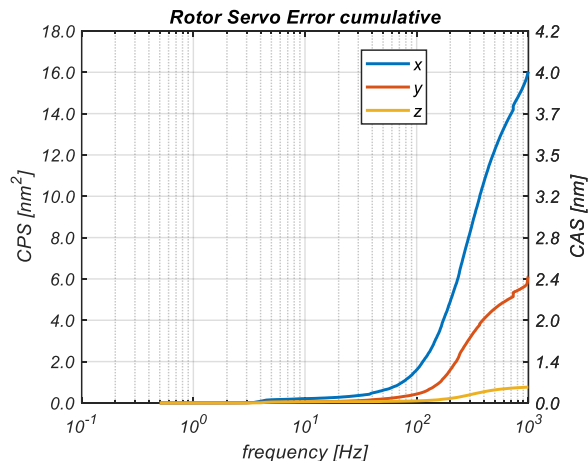
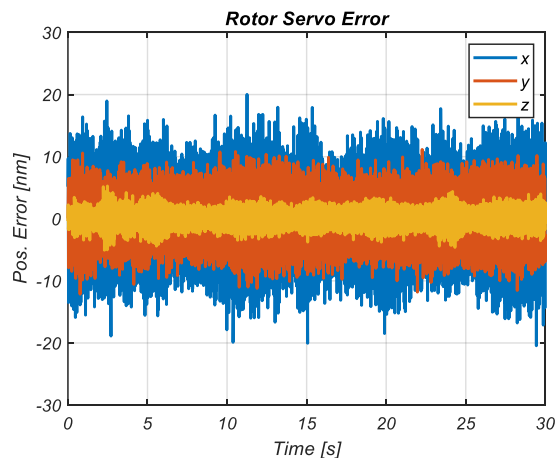
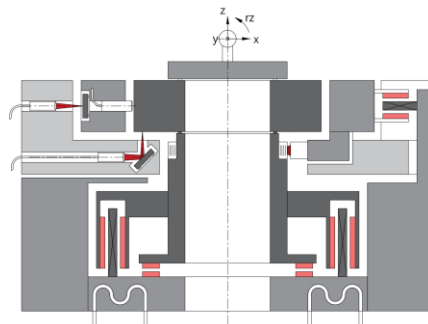
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Servo positioning error

1st results

Stand still performance at $R_z = \text{fixed}$



Servo positioning error

X: 4 nm_{RMS}

Y: 2.4 nm_{RMS}

Z: 0.9 nm_{RMS}

Frequency range

0.3...1000 Hz

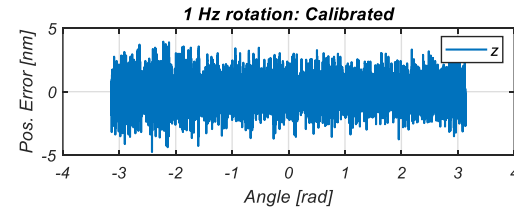
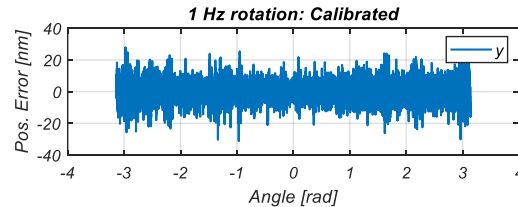
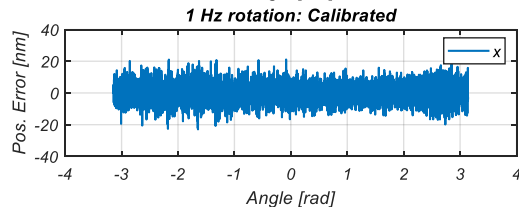
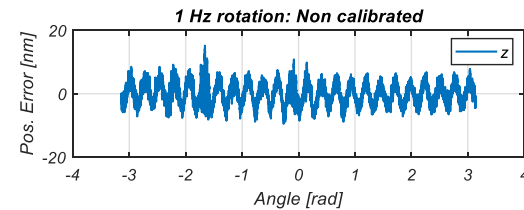
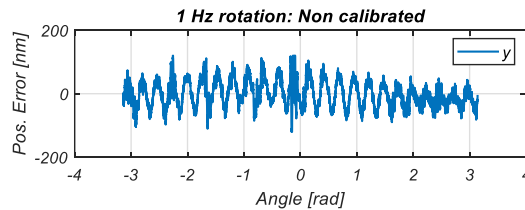
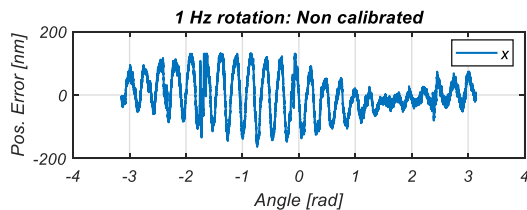
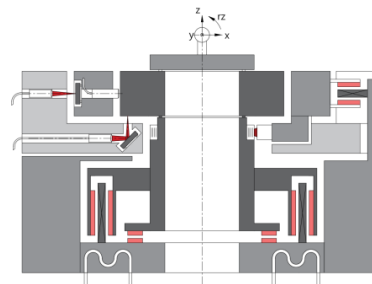
Positioning performance Rz = 1 Hz (1st results)

Servo positioning error

Rz rotation (centric) at 1 Hz

Without actuator calibration and after calibration

Results are comparable to stand-still



x,y : 3...4 nm_{RMS}

z : < 1 nm_{RMS}



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